

1 **Convective Transport of Peroxides by Thunderstorms Observed over the**
2 **Central U.S. during DC3**
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41 **Key Points:**

42 1. Peroxide scavenging efficiencies derived from measurements

43 2. Hydrogen peroxide is readily removed by storms

44 3. Methyl hydrogen peroxide scavenging correlated with ice, entrainment and lightning-NO_x

45 **Abstract**

46 One of the objectives of the Deep Convective Clouds and Chemistry (DC3) field experiment was
47 to determine the scavenging of soluble trace gases by thunderstorms. We present an analysis of
48 scavenging of hydrogen peroxide (H_2O_2) and methyl hydrogen peroxide (CH_3OOH) from six
49 DC3 cases that occurred in Oklahoma and northeast Colorado. Estimates of H_2O_2 scavenging
50 efficiencies are comparable to previous studies ranging from 79-97% with uncertainties of 5-
51 23%. CH_3OOH scavenging efficiencies ranged from 12-84% with uncertainties of 15-67%. The
52 wide range of CH_3OOH scavenging efficiencies is surprising, as previous studies suggested that
53 CH_3OOH scavenging efficiencies would be $<10\%$. Cloud chemistry model simulations of one
54 DC3 storm produced CH_3OOH scavenging efficiencies of 26-61% depending on the ice retention
55 factor of CH_3OOH during cloud drop freezing, suggesting ice physics impacts CH_3OOH
56 scavenging. The highest CH_3OOH scavenging efficiencies occurred in two severe thunderstorms,
57 but there is no obvious correlation between the CH_3OOH scavenging efficiency and the storm
58 thermodynamic environment. We found a moderate correlation between the estimated
59 entrainment rates and CH_3OOH scavenging efficiencies. The production of nitric oxide from
60 lightning may influence CH_3OOH convective outflow mixing ratios by reducing CH_3OOH
61 production because methyl peroxy radical reacts with nitric oxides instead of hydroperoxy
62 radical. However, parcel model simulations with added nitric oxide do not differ from those
63 without a nitric oxide source. To determine why CH_3OOH can be substantially removed from
64 storms, future studies should examine effects of entrainment rate, retention of CH_3OOH in
65 frozen cloud particles during drop freezing, and lightning- NO_x production.

66

67 1. Introduction

68 To understand the radiative impact of ozone in the upper troposphere (UT), ozone chemical
69 sources in the UT must be quantified. Ozone (O_3) is produced by the reactions between peroxy
70 radicals (e.g. hydroperoxy and methyl hydroperoxy radicals, HO_2 and CH_3OO , respectively) and
71 nitric oxide (NO) to form nitrogen dioxide (NO_2), which subsequently photodissociates to form
72 O_3 . Thus, odd hydrogen ($HO_x = OH + HO_2$; OH is hydroxyl radical) and nitrogen oxides ($NO_x =$
73 $NO + NO_2$) are key precursors to O_3 . Although the primary formation of HO_x radicals is from O_3
74 photodissociation, oxidation of volatile organic compounds (VOCs), as well as their
75 photodissociation, is also important. A source of these VOCs and NO_x in the UT is in convective
76 outflow regions, where VOCs are transported from the boundary layer (BL) to the UT and NO_x
77 is formed from lightning. However, many key HO_x precursors, including formaldehyde (CH_2O),
78 hydrogen peroxide (H_2O_2), and methyl hydrogen peroxide (CH_3OOH), are soluble and can be
79 partially removed from the atmosphere via dissolution into cloud drops that grow into rain, snow,
80 graupel, and hail precipitating to the ground. Quantifying the fraction of HO_x precursors that are
81 scavenged (or conversely transported to the UT) improves the estimation of O_3 production in
82 convective outflow regions. In this paper, we determine the scavenging efficiencies (SE) of H_2O_2
83 and CH_3OOH based on aircraft measurements obtained during the Deep Convective Cloud and
84 Chemistry (DC3) field experiment [Barth et al., 2015]. Fried et al. [2015] perform a similar
85 analysis for CH_2O while Bela et al. [2015] evaluate the convective transport of nitric acid, H_2O_2 ,
86 CH_2O , sulfur dioxide, and CH_3OOH in a 3-dimensional cloud chemistry model with
87 observations, and calculate the fraction of these species removed for four DC3 thunderstorm
88 cases.

89

90 Previous studies suggest convective transport of HO_x precursors play an important role in
91 controlling O₃ mixing ratios in the UT. Measurements of UT HO_x during the NASA STRAT
92 (1996) campaign occasionally exceeded theoretical estimates of HO_x concentrations, suggesting
93 an additional source of UT HO_x that was proposed to be convective transport of CH₂O, H₂O₂,
94 and CH₃OOH [Jaegle et al., 1997; Prather and Jacob, 1997; Wennberg et al., 1998].
95 Measurements from the NASA PEM-Tropics (1999) campaign revealed an enhancement of
96 CH₃OOH and a lack of enhancement of H₂O₂ in aged convective outflow over the tropical
97 Pacific, supporting the importance of convective transport for sources of hydrogen oxide radicals
98 in the upper troposphere [Ravetta et al., 2001]. Cohan et al [1999] estimated that H₂O₂ had 55-
99 70% scavenging efficiency based on measurements of tropical oceanic convection, while
100 CH₃OOH showed no apparent scavenging. Peroxide measurements from the INTEX-A field
101 campaign revealed that H₂O₂ was depleted while CH₃OOH was enhanced in convective outflow
102 regions compared to the background UT [Snow et al., 2007]. These prior measurements in
103 STRAT, PEM Tropics-B, and INTEX-A did not gather simultaneous inflow and outflow trace
104 gas measurements of convection to allow for estimates of peroxide scavenging. An
105 intercomparison study of cloud-scale chemistry models [Barth et al., 2007b] showed a large
106 variation in predictions of CH₂O and H₂O₂ that depended on whether or not the trace gas was
107 retained in frozen particles (snow, graupel or hail).

108

109 Other previous studies have indicated an unexpected reduced amount of CH₃OOH in the marine
110 boundary layer impacted by clouds compared to the reduction that would be expected due to gas-
111 phase photochemistry. Fried et al. [2003] discuss conditions at very low NO mixing ratios (< 5
112 pptv) where box model calculations predicted CH₃OOH mixing ratios to be 2-3 times greater

113 than nearby CH_3OOH observations. While we expect CH_3OOH to be higher at low NO mixing
114 ratios than at high NO, the theoretical estimates are much greater than observed, suggesting that
115 additional losses reduce CH_3OOH in reality. In the DC3 environment, NO mixing ratios were
116 rarely (if at all) this low. However, the reverse situation could exist where increases in NO
117 mixing ratios from lightning production enable peroxy radicals to react with NO instead of with
118 each other, thereby preventing the formation of peroxides.

119

120 Although H_2O_2 is highly soluble, its partitioning between gas and aqueous phases, as well as that
121 for CH_3OOH , should be in Henry's law equilibrium based on theoretical calculations and
122 analysis of field measurements [Barth et al., 1989; MacDonald et al., 1995]. Because the Henry's
123 law equilibrium coefficients for H_2O_2 are over two orders of magnitude higher than those of
124 CH_3OOH , we expect that more H_2O_2 than CH_3OOH will be removed by cloud and precipitation
125 than CH_3OOH . However, we will show that CH_3OOH is sometimes removed more than
126 expected, even as much as H_2O_2 .

127

128 In this paper we examine the behavior of CH_3OOH and H_2O_2 observed during DC3. The
129 scavenging efficiencies of H_2O_2 and CH_3OOH are derived from measurements of these
130 peroxides and tracers of transport that were collected during the DC3 field experiment. The DC3
131 campaign and the instrument techniques used in the analysis are described in the next section.
132 We then present the analysis method for determining each storm's entrainment rate and the
133 peroxide scavenging efficiencies. We also use cloud-resolved 3-dimensional and box model
134 simulations to investigate physical and chemical processes affecting the peroxide scavenging.
135 Results for six DC3 storm cases are presented. In addition to discussing the uncertainties of the

136 calculations, we show how the peroxide scavenging efficiencies vary with some key storm
137 parameters, including the storm physics and chemistry.

138

139 **2. Methods**

140 **2.1 Observations**

141 The DC3 field experiment took place in May and June 2012, sampling thunderstorms in
142 northeast Colorado, west Texas to central Oklahoma, and northern Alabama. Ground-based
143 facilities documented the storm kinematics, physical structure, and lightning location. Three
144 aircraft, the NASA DC-8, the NSF/NCAR Gulfstream V, and the DLR Falcon 20, sampled the
145 inflow and outflow regions of the storms to quantify the composition of these regions. Barth et
146 al. [2015] present further details on the DC3 field experiment. In this paper, we utilize the data
147 from the NASA DC-8 aircraft to examine the scavenging of hydrogen peroxide and methyl
148 hydrogen peroxide in thunderstorms. While NSF/NCAR GV peroxide data are also available,
149 reconciling differences between the DC-8 and GV peroxide measurements are beyond the scope
150 of this paper. The DC-8 data are analyzed because the DC-8 flew in both inflow and outflow
151 regions for each case analyzed (whereas the GV flew most often in outflow regions).

152

153 The DC8 aircraft was extensively instrumented with trace gas and aerosol instruments [Barth et
154 al., 2015]. A list of the data and instruments used in this study is given in Table 1. Horizontal
155 winds, temperature, and pressure measurements on the DC-8 were obtained via the
156 meteorological measurement system (MMS). Ice water content (IWC) was measured onboard the
157 DC-8 aircraft by the SPEC 2-dimensional Stereo (2DS) probe [Lawson et al., 2006].

158

159 On the DC-8 aircraft H₂O₂ and CH₃OOH were measured using time-of-flight (ToF-CIMS) mass
160 filter and tandem quadrupole mass filter (T-CIMS) chemical ionization mass spectrometers
161 (CIMS), respectively. The rapid-scan collection of the ToF-CIMS instrument provides high
162 temporal resolution (1 Hz or faster) and simultaneous data products for all masses [Nguyen et al.,
163 2015]. The T-CIMS provides parent-daughter mass analysis, enabling measurement of
164 compounds precluded from quantification by a single mass analyzer CIMS due to mass
165 interferences (e.g. CH₃OOH) or the presence of isobaric compounds (e.g. isoprene oxidation
166 products) [Paulot et al., 2009; St. Clair et al., 2010]. Calibrations for H₂O₂ and CH₃OOH are
167 performed once per hour during flight using calibration standards for H₂O₂ (evolved from urea-
168 hydrogen peroxide) and CH₃OOH (from a diffusion vial). Note that the uncertainties for H₂O₂
169 (>50%) and CH₃OOH (~80% at low altitude and ~40% at high altitude) are high and contribute
170 the largest uncertainty to the analysis performed in this study.

171

172 The non-methane hydrocarbons n-butane, i-butane, n-pentane, and i-pentane are used to estimate
173 the entrainment rate for each storm. On the DC-8, these hydrocarbons were measured using the
174 whole air sampler (WAS), which pumps a sample of air into a previously evacuated canister with
175 an approximately 1 minute fill time (up to 2 minutes at high altitude) that is analyzed in the
176 laboratory by gas chromatography [Colman et al., 2010; Simpson et al. 2010]. Sampling
177 frequency is variable, but is typically every 2 to 5 minutes.

178

179 Aircraft measurements of OH, HO₂, sulfur dioxide (SO₂), NO, NO₂, and methyl peroxy nitrate
180 (MPN) are used in assessing whether CH₃OOH scavenging efficiencies are correlated with these
181 trace gases or to examine the gas-phase CH₃OOH production. The HO_x radicals, OH and HO₂,

182 were measured by the Pennsylvania State University Airborne Tropospheric Hydrogen Oxides
183 Sensor (ATHOS), which is a laser induced fluorescence technique [Faloona et al., 2004]. SO₂ is
184 measured with the Georgia Institute of Technology Chemical Ionization Mass Spectrometer
185 (CIMS) [Kim et al., 2007]. NO and NO₂ were measured with ozone-induced chemiluminescence
186 and ultra-violet photolysis of NO₂ to NO followed by ozone-induced chemiluminescence,
187 respectively [Pollack et al., 2011]. The NO₂ data before June 11, 2012 are from the University of
188 California – Berkeley thermal dissociation-laser induced fluorescence (TD-LIF) instrument
189 [Thornton et al., 2000; Nault et al., 2015]. Methyl peroxy nitrate mixing ratios were also
190 measured with the TD-LIF instrument as described by Nault et al. [2015].

191

192 Next Generation Weather Radar (NEXRAD) program Weather Surveillance Radar – 1988
193 Doppler (WSR-88D) data [Crum and Alberty, 1993] are used to understand the storm structure
194 and to estimate the distance of the DC-8 aircraft sampling the outflow from the nearest storm
195 core. Data from multiple radars, which are S-band (10 cm wavelength) radars, are processed to
196 produce 3-dimensional composites following the procedure described in Homeyer [2014] and
197 updated in Homeyer and Kumjian [2015]. Radiosonde data from soundings launched in the pre-
198 storm environment are used to determine the thermodynamic environment of the storm.
199 Radiosondes in Colorado are from the NCAR Mobile Integrated Sounding System and those in
200 Oklahoma from the National Severe Storms Laboratory (NSSL). The National Weather Service
201 North Platte sounding was used for the May 18 storm observed in southwest Nebraska. The
202 convective available potential energy (CAPE), 0-6 km vertical wind shear, depth from cloud
203 base to the freezing level, and depth from the freezing level to the -40°C isotherm were

204 calculated from the soundings. The CAPE is determined using mixed layer mean temperature,
205 where the mixed layer is defined between the surface and 100 hPa above the surface.

206

207 Six case studies were chosen from the DC3 dataset (Table 2) based on the type of convection and
208 the availability of DC-8 inflow and outflow data. Four of these cases were in the northeast
209 Colorado and southwest Nebraska region, and two were in Oklahoma. The cases are primarily
210 severe convection, with CAPE ranging from 900 to 3100 J kg⁻¹, and 0-6 km vertical wind shear
211 range of 12-24 m s⁻¹. The depth of the cloud where T > 0°C (where only liquid water cloud
212 physics occurs) varies substantially among storms. The Colorado convective storms have much
213 shallower depths between cloud base and the freezing level than Oklahoma convection, but this
214 depth increases from mid-May to late June. The depth from the freezing level to T = -40°C,
215 which is the temperature where cloud drops homogeneously freeze, is fairly consistent among
216 storms with depths from 4900 to 5200 m for Colorado storms and ~5800 m for Oklahoma
217 storms.

218

219 **2.2 Analysis Method**

220 Calculations of scavenging efficiencies from aircraft observations have been done previously by
221 using a multi-component mixture model. Cohan et al. [1999] considered two components, one
222 being the inflow region and the second being the upper troposphere where the convective
223 outflow resides. Borbon et al. [2012] used three components (BL, free troposphere, and UT) and
224 Yang et al. [2015] used four components (BL, buffer layer, clean layer, and UT, where the buffer
225 layer extends from the BL to 7 km altitude and the clean air layer extends from 7 km to 9.5 km
226 where the UT layer begins), adding entrainment of free troposphere air. Luo et al. [2010]

227 estimated entrainment in every 1 km layer of the deep convection. Here, and in Fried et al.
228 [2015], we combine the methods of these previous studies to determine the scavenging
229 efficiencies of trace gases.

230

231 Measurements from the inflow and outflow regions of the storm, as well as the free troposphere,
232 were used to compute the scavenging efficiencies. The DC-8 aircraft gathered these observations
233 by first sampling the inflow BL composition at several altitudes including a flight leg above the
234 BL top, then spiraling up to the anvil outflow region where several across-anvil passes were
235 made (Figure 1). Often the anvil passes were several kilometers downwind of the storm core tops
236 in order to keep the aircraft in a safe location from damaging hail and turbulence. Thus, some
237 degree of anvil dilution and chemistry is imparted on the trace gas mixing ratios before the DC-8
238 aircraft collects the measurements. To minimize the impact of dilution and chemistry, we use
239 outflow data that are closest to the storm core tops. Fried et al. [2015] employed a similar data
240 analysis, but instead used 1-minute averaged data in the outflow flight segments to extrapolate
241 back to the storm core top.

242

243 The aircraft sampling of the inflow and outflow regions was found by identifying flight segments
244 where horizontal winds showed air flowing into the storm within the boundary layer and air
245 flowing away from the storm cores in the anvil. Besides the physical location of the plane, the
246 chemical signatures of CO, hydrocarbons, and IWC were used to identify these flight legs.
247 Figure 2 illustrates the outflow legs used in the analysis for the six convection cases. For each
248 case, 20 minutes of the DC-8 flight track is plotted over the column maximum radar reflectivity.
249 The DC-8 flight track is colored by the magnitude of the CH₃OOH 30-s averaged mixing ratio.

250 The wind vectors (data from the DC-8) are plotted for the segment of the flight track used for the
251 outflow analysis. The inflow and outflow times for each of the cases are listed in Table 3. The
252 distance between the aircraft and storm cores varied among the different storm cases, with some
253 cases (e.g. May 29 in Figure 2b) just a few km from the cores developing in the anvil region and
254 others (e.g. June 22 in Figure 2f) nearly 100 km from the storm core.

255

256 Once the inflow and outflow time periods were identified, the average mixing ratios for several
257 trace gases were calculated. In some cases, mixing ratios were not available because of in-flight
258 calibration of the instrument. For example, on 18 May 2012, the inflow CH_3OOH mixing ratio
259 was estimated based on nearby flight legs. Specifically for this case, an estimate of the CH_3OOH
260 at 1.68 km was obtained by dividing the H_2O_2 mixing ratio at 1.68 km by the H_2O_2 to CH_3OOH
261 ratio at 2.57 km (which is ~ 1.2).

262

263 To obtain information on air entraining into the storm, a vertical profile of cloud-free data from
264 the storm region was obtained. Stratospheric air was omitted by removing times where the O_3 to
265 CO ratio was greater than 1.25. This method may not remove all of the data points with
266 stratosphere influence because of mixing of air caused by the thunderstorms as described in
267 recent studies [Schroeder et al., 2014; Huntrieser et al., 2015a,b]. Also removed from these
268 profiles were measurements of other unique features such as biomass burning plumes. These
269 were removed by restricting the time frame for the profiles, which was determined from the high
270 CO mixing ratios. Most of the cloud-free profiles are based on the DC-8 spiral from the
271 boundary layer to the upper troposphere. The data were binned into 1 km altitude ranges.
272 Missing data (because of in-flight calibrations and zeros) were filled in by interpolating to the

273 altitude of the missing data from the averages found above and below that altitude, and
274 extrapolating to the lowest or highest altitude if needed. Figure 3 shows cloud-free vertical
275 profiles of H₂O₂, CH₃OOH, n-butane, i-butane, n-pentane, and i-pentane for the six cases.

276

277 Cloud-free profiles of n-butane, i-butane, n-pentane, and i-pentane were used to estimate the
278 entrainment rate. These VOCs have chemical lifetimes (3-5 days) much longer than the time for
279 convective transport from the BL to the UT (typically 10-15 minutes [Skamarock et al., 2000])
280 and transport downwind to the aircraft (typically 30-45 minutes). Long chemical lifetimes and
281 very low solubility allow these VOCs to be markers of transport only. Fried et al. [2015] further
282 discuss the merits of using these tracers. The entrainment model follows an air parcel from just
283 below cloud base (CB), where that air has a VOC mixing ratio representing the BL, to the
284 location of the aircraft anvil measurements, where the VOC mixing ratio is a combination of the
285 VOC from the BL and the cloud-free (CF) VOC mixing ratios that are entrained into the storm.
286 The entrainment rate E (% km⁻¹) is found by calculating the VOC mixing ratio at 1-km altitude
287 bins from just below cloud base to the height of the aircraft measurements. For example, the
288 VOC mixing ratio at one km above cloud base ($VOC(z_{CB+1})$) is a combination of the VOC
289 mixing ratio at cloud base ($VOC(z_{CB})$) and the VOC in the cloud-free air at one km above cloud
290 base $VOC_{CF}(z_{CB+1})$ based on the fraction entrained. This equation can be generalized by the
291 following equation,

292

$$293 \quad VOC(z) = E VOC_{cf}(z) + (1 - E) VOC(z - 1) \quad (1)$$

294

295 where $VOC(z)$ is the n-butane, i-butane, n-pentane, or i-pentane mixing ratio in the updraft at
296 each 1-km altitude z (km), $VOC(z-1)$ is the VOC mixing ratio at 1 km below the altitude z , and

297 $VOC_{cf}(z)$ is the average VOC mixing ratio in the cloud-free region at each 1-km altitude z . To
298 determine E , equation 1 was iterated until the calculated VOC mixing ratio at the height of the
299 aircraft outflow measurements and the measured VOC mixing ratio in the outflow region
300 matched within 1-10%. This procedure was conducted for all four VOCs and the average of
301 these derived entrainment rates were used to calculate the scavenging efficiency. The highest to
302 lowest entrainment rates give the range of entrainment rates for each storm and are used in
303 expressing the entrainment rate uncertainty. It is assumed that the entrainment rate is the same at
304 every 1 km altitude, however we estimate the impact of this assumption by utilizing variable
305 entrainment rates determined in the WRF simulation for the 29 May DC3 case in Section 3.

306

307 The first step in obtaining the scavenging efficiency of a soluble trace gas having mixing ratio
308 C_{sol} is to determine C_{sol} at the height of the aircraft outflow measurements ($C_{sol}(z=top)$) if it were
309 only transported (i.e. there is no dissolution into cloud particles and chemistry does not affect the
310 mixing ratio of C_{sol}). $C_{sol}(z=top)$ is found by using equation 1 with H_2O_2 or CH_3OOH in place of
311 the VOC and using the average entrainment rate. The scavenging efficiency SE (%) is found by
312 calculating the difference between the soluble trace gas mixing ratio measured from the aircraft
313 $C_{sol}(outflow)$ and the estimated transported mixing ratio at the height of the aircraft $C_{sol}(z=top)$
314 using,

315

$$316 \quad SE = 100 \frac{C_{sol}(z = top) - C_{sol}(outflow)}{C_{sol}(z = top)} \quad (2)$$

317

318 The uncertainty for $C_{sol}(outflow)$ is the average uncertainty of the measurements in the outflow
319 flight leg. The uncertainty for the scavenging efficiency and $C_{sol}(z=top)$ are found by the
320 quadrature method (Taylor, 1982).

321
322 While equation 2 is defining the scavenging efficiency, which is viewed as the physical removal
323 of a trace gas via dissolution and rain out, the equation actually encompasses all physical and
324 chemical processes occurring between the inflow and outflow regions sampled by the aircraft.
325 Thus, there can be physical removal, chemical destruction or even a reduction in chemical
326 production. An example of the last process, mentioned in the introduction and discussed in
327 Section 4, is the reduction in peroxide formation because the peroxy radicals react with NO to
328 form NO₂ and CH₂O instead of reacting with each other to form the peroxides.

329

330 **2.3 Description of Cloud-Resolving Scale Model Simulations**

331 The 29 May 2012 northern Oklahoma storm has been simulated with the Weather Forecasting
332 and Research model coupled with Chemistry (WRF-Chem [Grell et al., 2005]). Bela et al. [2015]
333 give a full description of the model configuration and simulation results. Table 4 provides
334 information on the WRF-Chem configuration. The model domain is centered on northern
335 Oklahoma using 1-km horizontal grid spacing and 88 vertical levels to 50 hPa (~20 km). The
336 cloud resolving grid spacing allows for explicit representation of transport and wet deposition in
337 the deep convection. The wet deposition scheme [Neu and Prather, 2012] estimates wet removal
338 of soluble trace gases from the gas phase. This scheme estimates trace gas removal by
339 multiplying the effective Henry's Law equilibrium aqueous concentration by the net
340 precipitation formation (conversion of cloud water to precipitation, minus evaporation of

341 precipitation). In mixed-phase conditions ($258 \text{ K} < T < 273 \text{ K}$), the Neu and Prather [2012]
342 scheme estimates a fraction of the dissolved gas to be retained in the frozen hydrometeors. The
343 retention fraction of H_2O_2 and CH_3OOH is set to 0.64 and 0.01, respectively, in accordance with
344 laboratory values compiled by Leriche et al. [2013]. Other soluble trace gases (CH_2O , HNO_3 ,
345 and SO_2) also use retention factors recommended by Leriche et al. [2013], while all other trace
346 gases are completely degassed from the condensed phase. Sensitivity simulations were
347 conducted to explore the effect of the retention factor on trace gas scavenging.

348

349 In addition to the simulations that included wet deposition, a simulation without wet deposition
350 was performed. The scavenging efficiencies (SE) are then calculated from these results using the
351 following equation.

352

$$353 \quad SE = 100 \frac{(C_{noscav} - C_{scav})}{C_{noscav}} \quad (3)$$

354 where C_{noscav} and C_{scav} are average model mixing ratios of soluble trace gas C near the storm core
355 as defined by the eastern (i.e., downwind) 40 dBZ maximum reflectivity contour. This location
356 was chosen based on the analysis method of the observations outlined above. For the 29 May
357 DC3 case, the DC-8 measurements were obtained near storm cores with reflectivity $> 40 \text{ dBZ}$
358 (Figure 2b). The mixing ratios of the trace gases were averaged in the convective outflow
359 altitudes (9.43-11.59 km).

360

361 In another simulation, 20 tracers representing air in each 1-km altitude layer of the atmosphere
362 from the surface to the top of the model ($\sim 20 \text{ km}$). These layer tracers were set to a value of 1.0
363 in their respective layer for a 10-minute time period (0010-0020 UTC 30 May 2012) and

364 analyzed 2 hours after the initialization of the tracer at 0200 UTC 30 May 2012 to allow time for
365 boundary layer air to reach the outflow location. The results were analyzed to determine the
366 percent contribution of each layer to the modeled storm core top as defined above. These percent
367 contributions from each layer (Table 5) were used as the entrainment rate for calculations of
368 scavenging efficiency from the aircraft observations to compare results from an average
369 entrainment rate with those from an altitude-varying entrainment rate in Section 3.

370

371 **2.4 Box Model Calculations**

372 The gas-aqueous chemistry box model described by Barth et al. [2003] is used to analyze the
373 chemistry within the updraft regions of a severe thunderstorm. The box model has been modified
374 to include the non-methane hydrocarbon gas-phase chemistry described by Kim et al. [2012].
375 The aqueous-phase chemistry represents only S(IV), O₃, H₂O₂, and CH₂O chemistry [Barth et al.,
376 2007a]. Other soluble VOC trace gases, e.g. organic aldehydes, peroxides, and nitrates, also
377 partition into the aqueous phase following Henry's Law equilibrium, but do not undergo
378 aqueous-phase chemistry. The coefficients for Henry's Law are from Sander [2015] and Sander
379 et al. [2011]. Photolysis rates are appropriate for 36°N beginning at 00 UTC (1900 local time),
380 matching the time of the storm observations. The photolysis rates vary with altitude and are
381 modified by cloud scattering assuming a cloud optical depth of 500, cloud base of 2 km and
382 cloud top of 15 km. The photolysis rates are less than their clear sky values throughout the
383 simulation as depicted by the cloudy to clear sky H₂O₂ photolysis rate ratio in Figure 4b.

384

385 The box model has also been modified to have varying liquid water content, temperature,
386 pressure, and altitude, which are prescribed using results from the WRF-Chem simulation at 00

387 UTC 30 May 2012. Values are averages at each model level within the 36°N-37°N and 99°W-
388 97°W latitude and longitude region and where vertical velocity in the column exceeds 5 m s⁻¹.
389 The resulting cloud hydrometeor vertical profiles are shown in Figure 4a. For the box model
390 simulations we prescribe only the cloud liquid water content and exclude the water content from
391 precipitation. From Figure 4, it is evident that much of the condensed water is in the
392 precipitation, primarily as hail, for this updraft region. Because the box model calculations are a
393 function of time, the prescribed time coordinate is converted to an altitude coordinate so that the
394 chemistry of a hypothetical rising air parcel can be determined. The air parcel begins at the 1.16
395 km altitude (near cloud base), solves for only gas-phase chemistry for 10 minutes to allow the
396 radicals to reach approximate photochemical equilibrium, then is lifted to higher altitudes
397 assuming a 3 m s⁻¹ updraft. At ~14 km where the WRF-Chem updraft velocities are ~0 m s⁻¹, the
398 artificial lifting of the box is stopped. The 14 km altitude is above the cloud water region of the
399 storm (Figure 4); the top of the cloud water region is 10.9 km. Thus, the air parcel undergoes just
400 gas-phase chemistry between 10.9 and 14 km.

401

402 To determine if H₂O₂ and CH₃OOH would be depleted if only gas-phase chemistry were
403 occurring, a box model simulation with no liquid water was performed. Figure 4 shows that
404 H₂O₂ and CH₃OOH have similar mixing ratios at cloud base (2.2 ppbv for H₂O₂ and 1.46 ppbv
405 for CH₃OOH). Thus, for the conditions of the box model simulation, both peroxides are not
406 produced by the gas-phase chemistry. A second simulation with the prescribed LWC show that
407 in the cloud water region (2-11 km altitude) gas-phase H₂O₂ is rapidly depleted, with mixing
408 ratios reduced to <0.2 ppbv in the mixed cloud region (4-11 km altitude). Note that solubility
409 constants increase as temperature decreases, allowing more of the soluble trace gas to partition

410 into the aqueous phase. Gas-phase CH_3OOH mixing ratios also decrease, but by <10% of the
411 gas-phase only simulation. At the top of the cloud water region, the peroxides in the aqueous
412 phase return to the gas phase because of the lack of liquid water. In an actual cloud the cloud
413 water is more likely being collected by precipitating cloud particles and freezing. Thus, what is
414 shown in Figure 4 is akin to the trace gases being degassed from all cloud particles. In summary,
415 simple partition theory based on Henry's law equilibria and gas- and aqueous-phase chemistry
416 suggests substantial depletion of gas-phase H_2O_2 and small depletion of CH_3OOH . Gas-phase
417 chemistry alone does not deplete either H_2O_2 or CH_3OOH appreciably during transit from cloud
418 base to cloud top.

419

420 **3. Results**

421 Average mixing ratios for H_2O_2 and CH_3OOH measured during the DC8 flight inflow and
422 outflow time periods are listed in Table 6. The mixing ratios in the inflow region are always
423 higher than those in the outflow for both peroxide species, indicating that net production of
424 peroxides within the storm is not occurring. The inflow mixing ratios vary from case to case,
425 suggesting a dependence on vicinity to anthropogenic sources and time of year. The 18 May and
426 22 June storms, with lower H_2O_2 mixing ratios, both occurred near the Wyoming-Colorado-
427 Nebraska border further from the Front Range urban region than the 2 June and 6 June Colorado
428 cases. The average NO_x mixing ratios for the 29 May, 2 June, 6 June, and 16 June inflow air
429 were 400-650 pptv, whereas that for the 22 June storm was ~260 pptv (the inflow NO_x mixing
430 ratio for the 18 May storm was not measured due to instrument issues). The outflow mixing
431 ratios also have some variability among the different storm cases. The uncertainties for the
432 average values can be quite large, ranging from 50-60% and 77-84% for H_2O_2 and CH_3OOH ,

433 respectively, in the boundary layer inflow air and 80-175% and 49-70% for H₂O₂ and CH₃OOH,
434 respectively, in the outflow air.

435

436 The mixing ratios for the butanes and pentanes in the inflow air (Table 7) vary from storm to
437 storm, but the variation is not correlated to the variation found for the peroxides. Higher mixing
438 ratios in both the inflow and outflow air occur over Oklahoma than in Colorado, except for the
439 18 May case. The outflow mixing ratios are often much smaller than the inflow mixing ratios,
440 except for the 22 June outflow where mixing ratios are only slightly less than those in the inflow
441 suggesting less entrainment in the 22 June storm. Note that the 6 June case uses butane and
442 pentane mixing ratios extrapolated to the storm top as determined by Fried et al. [2015] because
443 the DC-8 mixing ratios from the outflow period listed in Table 5 have anomalously high butane
444 and pentane mixing ratios that are greater than the inflow mixing ratios. Instead of using DC-8
445 data from outflow near the edge of the storm (and quite far from the storm cores), we chose to
446 use the mixing ratios determined from a combination of DC-8 and GV data [Fried et al., 2015].

447

448 The i-butane/n-butane and i-pentane/n-pentane ratios also provide evidence that the air measured
449 by the DC-8 in the inflow region of the storms is connected to that sampled in the outflow region
450 in the storm anvils. Gilman et al. [2013] and Swarthout et al. [2013] explain that these ratios are
451 limited to a small range of values for a given source (e.g. cities, biomass burning emissions, oil
452 and gas emissions). However, the ratios from source to source varies, where the i-butane/n-
453 butane ratio is found to be 0.48 for U.S. cities, 0.26-0.27 for biomass burning emissions, 0.36-
454 0.69 for oil and gas emissions, and i-pentane/n-pentane ratio is 2.0 for U.S. cities, 0.31-0.37 for
455 biomass burning emissions, and 1-1.4 for oil and gas emissions in the Texas, Oklahoma, Kansas

456 region [Blake et al., 2015; Fried et al., 2015]. These ratios should be maintained for several hours
457 because their rate constants with OH are within 10-15% for n-butane and i-butane oxidation and
458 within 10% for n-pentane and i-pentane oxidation. The i-butane/n-butane and i-pentane/n-
459 pentane ratios for the inflow regions of all the storms analyzed for this study lie within the range
460 for oil and gas emissions as found by Blake et al. [2015] and Gilman et al. [2013] for the Texas,
461 Oklahoma, and Kansas region. This is not a surprising result because both Oklahoma and
462 northeast Colorado have active oil and gas operations. The i-butane/n-butane and i-pentane/n-
463 pentane ratios are fairly consistent between inflow air and outflow air for each storm, although
464 some differences occur possibly because the storm is entraining air with different i-butane/n-
465 butane and i-pentane/n-pentane ratios than the inflow region. Nevertheless, these ratios indicate
466 that the two air masses sampled are well connected between inflow and outflow of each storm.

467
468 Entrainment rates, as calculated via the method described in Section 2.2, range from $4.1\% \text{ km}^{-1}$
469 to $17.2\% \text{ km}^{-1}$ for the different storms analyzed (Table 8). The entrainment rate for 6 June was
470 obtained from Fried et al. [2015] because the VOCs measured by the DC-8 were anomalously
471 high in the outflow region. The entrainment rates for three of the cases are similar to those found
472 by Luo et al [2010] who used moist static energy profiles to determine entrainment rates of
473 $<10\% \text{ km}^{-1}$ for deep convective tropical, oceanic cumulus clouds. Moreover, the entrainment rate
474 for the May 29 storm is identical to that found by Fried et al. [2015]. The entrainment rate for the
475 June 22 storm is within the mutual precision limits of Fried et al. [2015] who estimated $3.1 \pm$
476 $1.1\% \text{ km}^{-1}$ compared to $4.8 \pm 0.9\% \text{ km}^{-1}$ in this study. The small difference for the June 22 storm
477 is expected since Fried et al. [2015] extrapolate their outflow data to estimate mixing ratios at
478 storm core top, which are generally higher than the average values closest to the storm core

479 employed here. If the entrainment rates reported in Table 8 are integrated for a 9 km depth, the
480 total storm entrainment rate range is 40-68%, which is similar to entrainment rates of
481 midlatitude, continental convection [Barth et al., 2007a; Thompson et al., 1994] and subtropical
482 convection [Scala et al., 1990]. The entrainment rates determined here tend to be smaller for
483 storms with higher 0-6 km vertical wind shear (Table 2), although the 16 June Oklahoma case
484 has a high vertical wind shear of $\sim 16 \text{ m s}^{-1}$ and a high entrainment rate. Both low-level vertical
485 wind shear and entrainment rate contribute to the storm intensity and longevity as they play a
486 role in the strength of the cold pool and tilt of the updraft [Weisman et al., 1988; Lee et al.,
487 2008].

488

489 The calculated scavenging efficiencies for H_2O_2 and CH_3OOH for each storm analyzed range
490 from 79% to 97% and 12% to 84%, respectively (Table 8). While there is some variability of
491 scavenging efficiency among storms for H_2O_2 , there is much more variability for CH_3OOH . The
492 H_2O_2 scavenging efficiencies estimated from DC3 storms are somewhat greater than those
493 previously found. Numerical modeling of a low-precipitation supercell observed in northeast
494 Colorado yielded a 57% H_2O_2 scavenging efficiency [Barth et al., 2007a]. Wang [2005]
495 estimated H_2O_2 scavenging efficiencies of 88-90% for tropical deep convection. Global
496 chemistry transport model simulations estimated that a soluble species with a Henry's Law
497 coefficient similar to H_2O_2 has a 90% scavenging efficiency in deep convection [Crutzen and
498 Lawrence, 2000]. Estimated H_2O_2 scavenging efficiency, based on boundary layer, convective
499 outflow, and UT background observations, for an oceanic, tropical convective storm is 55-70%
500 [Cohan et al., 1999]. CH_3OOH scavenging efficiencies for DC3 storms are also greater than past

501 results. Barth et al. [2007a] determined a 7% scavenging efficiency, while Cohan et al. [1999]
502 found no significant scavenging of CH₃OOH.

503

504 The most surprising result is the substantial scavenging of CH₃OOH for two of the storms (29
505 May and 6 June) of greater than 75%, which is much greater than what is expected based on
506 Henry's Law equilibrium between the gas and aqueous phases as shown in Section 2.4.
507 However, the cloud physics in deep convective clouds is much more complicated than the simple
508 model of a liquid-only cumulus cloud. The ice phase in deep convection interacts with the cloud
509 and rain drops through freezing and melting processes, and the fate of the dissolved trace gas is
510 uncertain when freezing occurs [Barth et al., 2001; 2007a], but is related to the value of the trace
511 gas Henry's Law and the time it takes a drop to freeze [Stuart and Jacobson, 2006]. Other storm
512 characteristics (e.g. entrainment) can also affect the scavenging rate of the trace gas. Some of
513 these effects will be discussed in the next section.

514

515 It is important to realize that the uncertainty in the estimated scavenging efficiencies is large and
516 is mostly a product of the uncertainties of the peroxide measurements. The peroxide uncertainties
517 are 50% or greater for H₂O₂ and ~80% for low altitude and 40% or greater for high altitude
518 CH₃OOH (Section 2, Table 6). The high uncertainties propagate to the scavenging efficiencies,
519 manifesting into 5-23% uncertainty in the H₂O₂ scavenging efficiency and 15-67% uncertainty in
520 the CH₃OOH scavenging efficiency. For CH₃OOH, there tends to be more uncertainty associated
521 with the lower scavenging efficiencies.

522

523 In addition to the measurement uncertainties, there are uncertainties associated with the analysis
524 method. While much care was invested in quantifying relevant values in inflow and outflow air,
525 there exists the possibility that the times chosen include air that was not processed by the deep
526 convection. A major assumption of the analysis is that the entrainment rate is constant for each
527 kilometer layer from cloud base to the top of the storm cell. To test this assumption, the WRF-
528 Chem model run using tracers described in Section 2.3 was analyzed to provide an altitude-
529 dependent entrainment rate (Table 5) for the 29 May severe convection case in Oklahoma. For
530 this case, the entrainment rate based on the hydrocarbon analysis was estimated to be 7.6%,
531 while the WRF-Chem model estimated an average entrainment rate for the 1-11 km altitude
532 range of 7.3%. Thus, the average entrainment rates based on these two methods are similar.
533 However, the model results give a variation of entrainment with height, with higher entrainment
534 in the first 2 kilometers near cloud base and near 7 km and the lowest entrainment from 3-5 km
535 altitude and above 9 km altitude (Table 5). By using the altitude-dependent entrainment rates for
536 estimating the scavenging efficiency, we obtain values of 89% and 80% scavenging for H₂O₂
537 and CH₃OOH, respectively. These values are similar to the 88% and 77% estimated by the
538 constant entrainment rate method and are well within the uncertainty.

539
540 A comparison of WRF-Chem simulations with and without wet deposition was done to estimate
541 scavenging efficiencies for the 29 May northern Oklahoma storm. Average H₂O₂ and CH₃OOH
542 mixing ratios at the eastern edge of the modeled storm core tops, which was defined in
543 longitude-latitude space by the column maximum radar reflectivity of 40 dBZ, were found for
544 each of the simulations. Bela et al. [2015] explore the sensitivity of the scavenging efficiency to
545 the retention of the dissolved trace gas in freezing drops. They find that the H₂O₂ scavenging

546 efficiency to be 100% with retention fractions into ice of 0.25, 0.5, 0.64, and 1.0 and $78\pm 11\%$ for
547 when there is no retention of dissolved trace gas in freezing drops. For CH_3OOH , Bela et al.
548 [2015] find the scavenging efficiency to be $26\pm 6\%$, $35\pm 7\%$, $39\pm 5\%$, $51\pm 4\%$, and $61\pm 3\%$ for
549 retention fractions of 0, 0.02, 0.25, 0.5, and 1.0, respectively. The model results with 100%
550 retention for CH_3OOH in ice give a CH_3OOH scavenging efficiency (61%) most similar to the
551 value calculated from observations (77%). In contrast, the simulation with 0% retention in ice
552 produced CH_2O mixing ratios in the convective outflow that best matched the observations
553 [Fried et al., 2015]. Further analysis is being done to investigate the potential role of aqueous-
554 phase chemistry on peroxide mixing ratios. These results suggest the retention of H_2O_2 and
555 CH_3OOH in freezing drops is an important contribution to scavenging of peroxides.

556

557 **4. Discussion**

558 Here, we seek to get an idea of what atmospheric processes contribute to the wide range of
559 CH_3OOH scavenging that can be used as guidance in future analysis. Both physical processes
560 and chemical transformations can affect the H_2O_2 and CH_3OOH mixing ratios in thunderstorms.
561 The thermodynamic environment in which the storms form determines the storm morphology.
562 However, key cloud physical processes affecting the soluble trace gases are the liquid water
563 content and the production of graupel and hail. As the air parcel is ingested and lofted to the top
564 of the storm and then carried into the anvil region, the soluble trace gases undergo chemical
565 transformations in both the gas and aqueous phases. All of these factors must be considered in
566 terms of understanding the estimated H_2O_2 and CH_3OOH scavenging efficiencies. Since derived
567 CH_3OOH scavenging efficiencies vary so much, the discussion focuses on CH_3OOH .

568

569 The thermodynamic environment is critical for determining the storm morphology and intensity.
570 Two important parameters of the thermodynamic environment are the convective available
571 potential energy (CAPE) and the low-level vertical wind shear [Weisman and Klemp, 1982]. For
572 DC3 storm cases, Barth et al. [2015] showed that the Alabama cases resided in the low shear and
573 low CAPE regime, the Oklahoma/Texas cases resided in the high shear and high CAPE regime,
574 while the Colorado cases resided between these two extremes. However, two Colorado cases had
575 both high vertical wind shear and high CAPE similar to the Oklahoma cases. Placing the
576 scavenging efficiencies in the context of the thermodynamic environment (Figure 5) shows that
577 there is no strong correlation of H_2O_2 scavenging efficiencies with CAPE and the 0-6 km vertical
578 wind shear. The same is true for CH_3OOH scavenging efficiencies, although the two highest
579 CH_3OOH scavenging efficiencies occur in severe storms with similar CAPE and vertical wind
580 shear parameters.

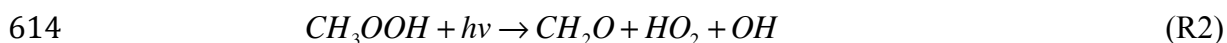
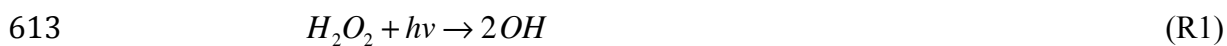
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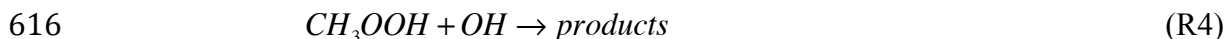
582 The morphology of the storm also depends on the depth of the warm cloud where only liquid
583 water resides and depth of the mixed phase region because the cloud physics processes differ in
584 these two regions. The Colorado storms have higher cloud bases than the Oklahoma storms
585 because the warm and dry boundary layers in the region require higher lifting condensation
586 levels. The Colorado storms have shallow warm cloud depths (Table 2), restricting the degree of
587 scavenging via collision and coalescence of cloud droplets. However, supercooled liquid water
588 can exist at temperatures down to 233 K (-40°C) and dissolution into the liquid from the gas
589 phase occurs much more readily at colder temperatures. Nevertheless, the calculated H_2O_2 and
590 CH_3OOH scavenging efficiencies showed no correlation with the warm cloud depth or depth of
591 cloud where cloud droplets exist. Further, the average ice water content (IWC) measured during

592 each outflow leg showed no correlation with the H₂O₂ and CH₃OOH scavenging efficiencies.
593 Fried et al. [2015] found the same lack of correlation between CH₂O scavenging efficiencies and
594 IWC and did not see substantial differences of CH₂O scavenging efficiencies between types of
595 storms except possibly the weak convection observed in Alabama that had a high CH₂O
596 scavenging efficiency.

597
598 The amount of entrainment estimated for each storm may affect the CH₃OOH scavenging
599 efficiency. For five out of the six storms, there is an increase in scavenging efficiency with a
600 decrease in entrainment (Figure 6). Entrainment brings into the storm free troposphere
601 background mixing ratios that are lower than those at the top of the boundary layer resulting in a
602 reduction in CH₃OOH mixing ratios in the updraft regions. When there is more entrainment,
603 more low mixing ratios are mixed into the updraft region than when entrainment rates are lower.
604 The possible importance of entrainment on convective outflow mixing ratios suggests that the
605 shape of the vertical profile of the peroxides may be important. For example, a rapid decrease in
606 mixing ratio from the top of the boundary layer into the free troposphere would decrease
607 CH₃OOH more than if the cloud-free mixing ratios remained elevated into the mid-troposphere
608 (e.g. June 16, Figure 3).

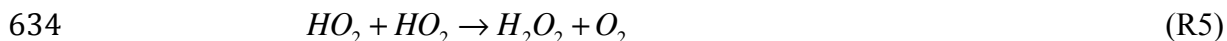
609
610 Another factor to consider is the chemistry that the peroxides experience as they are transported
611 from cloud base to the aircraft location in the anvil outflow region. Both H₂O₂ and CH₃OOH are
612 primarily destroyed by photolysis (R1, R2) and oxidation by OH (R3, R4).

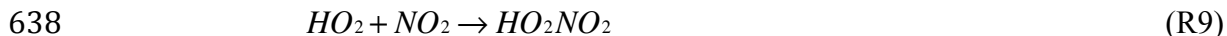




617 The rates of these reactions are altered by the presence of deep convection because the cloud
618 particles scatter incoming solar radiation. When the cloud is attenuating solar radiation causing
619 reduced photolysis rates and OH concentrations [Chang et al., 1987; Brasseur et al., 2002], the
620 photochemistry tends to proceed more slowly. However, near the top of cloud where it is much
621 brighter, the chemistry is accelerated. Because H₂O₂ and CH₃OOH are both produced and
622 destroyed by HO_x and photolysis rates, their gas-phase photochemistry is less certain when
623 clouds scatter radiation. Previous modeling studies showed a <5% effect on peroxide mixing
624 ratios caused by cloud modified photolysis rates for boundary layer clouds in a marine setting
625 [Barth et al., 2002]. However, Wang [2005] expected increases of H₂O₂ in the upper regions of
626 deep convection due to the decreased photolysis rates and lack of water in which H₂O₂ dissolves
627 and undergoes aqueous chemistry.

628
629 The production of H₂O₂ is primarily from the hydroperoxy radical self-reaction (R5). Similarly,
630 CH₃OOH is produced from methyl peroxy radical reaction with the hydroperoxy radical (R6).
631 However, NO reaction with the peroxy radicals and NO₂ reaction with peroxy radicals compete
632 with the peroxide production (R7-R10), causing less peroxide production at higher NO
633 concentrations.





640 In a thunderstorm, low NO conditions may exist in the inflow region of the storm, but as the air
641 parcel rises generation of NO from lightning would create a high NO situation. While the peroxy
642 radicals have other destruction reactions (e.g. $HO_2 + OH$, and reaction with other organic peroxy
643 radicals), their contribution to peroxy radical loss is much smaller than the reactions listed in R7-
644 R10. Comparing the loss of CH_3OO via reaction with HO_2 (R6) with those via reactions with NO
645 (R8) and NO_2 (R10) can illuminate whether the NO conditions are affecting the estimate of the
646 CH_3OOH scavenging efficiency. We can define the fraction of CH_3OO to produce CH_3OOH
647 ($F_{Prod_CH_3OOH}$) as,

648
$$F_{Prod_CH_3OOH} = \frac{k_6[HO_2]}{k_6[HO_2] + k_8[NO] + k_{10}[NO_2]} \quad (4)$$

649 This fraction can be estimated using the DC-8 aircraft data for NO, NO_2 , HO_2 , and temperature.
650 The calculated $F_{Prod_CH_3OOH}$ values are found to be < 1% because of the high NO_x mixing ratios,
651 which ranged from 0.7 to 2.5 ppbv, and low HO_2 mixing ratios (0.3 – 3.9 pptv) measured in the
652 outflow flight legs. Comparing $F_{Prod_CH_3OOH}$ to the CH_3OOH scavenging efficiency (Figure 7a)
653 shows for five of the six storms analyzed there is a strong correlation ($r^2 = 0.90$) between the two
654 parameters, with more CH_3OOH scavenged when its fraction produced is less. The one storm
655 that did not correspond well with this trend is the June 16, 2012 Oklahoma storm when outflow
656 measurements were taken near sunset (measured photolysis rates were 2 orders of magnitude
657 smaller than the other DC3 cases analyzed).

658

659 Reaction 10 produces methyl peroxy nitrate (MPN), which was measured by the TD-LIF
660 instrument on the DC-8. A comparison of average MPN data in the outflow region with the

661 CH₃OOH scavenging efficiencies shows no correspondence between the two parameters when
662 all the storms are included in the comparison, but a strong correspondence between the two
663 parameters when the data from 18 May and 6 June Colorado storms are omitted (Figure 7b).
664 MPN measurements from these two storms were below detection limit. Nevertheless, the
665 correlation shown in Figure 7b suggests that lightning-generated NO_x in the updraft region and
666 anvil is correlated with CH₃OOH mixing ratios in the anvil.

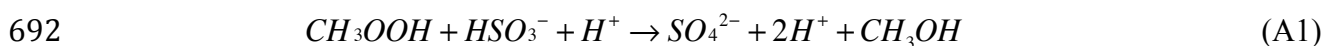
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668 To learn whether NO production from lightning could be a potential reason for CH₃OOH
669 depletion in thunderstorm anvils, the gas-aqueous photochemical box model was used. The
670 model began with the same conditions as described in Section 2.4 but had a NO emission
671 included representing lightning-NO_x production. The NO source was set to 10 pptv per time step
672 (10 s) from the altitude where T = 285 K to the altitude where T = 223 K. This profile is based
673 on the WRF-Chem results of NO mixing ratio in the updraft region. In Figure 8a, the NO vertical
674 profiles from the simulations without the “lightning-NO_x” source and with the “lightning-NO_x”
675 source are shown. The source of NO causes an increase of NO mixing ratios from ~0.1 ppbv to
676 ~1.2 ppbv. Even with the increase in NO mixing ratios, both gas-phase H₂O₂ and CH₃OOH
677 mixing ratios are unchanged from the simulations where the “lightning-NO_x” source was not
678 included (Figure 8b), although the change in CH₃OOH mixing ratios does show a <5 pptv
679 decrease. Despite the null result from the parcel model calculations, the correlations shown
680 above suggest that chemistry may play a role in affecting peroxide mixing ratios and cloud-
681 resolving chemistry models could be used to examine this further.

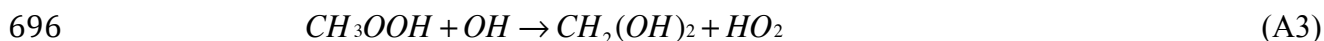
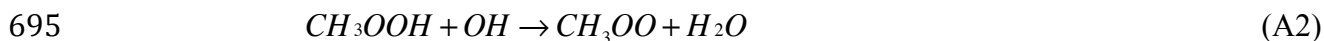
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683 The results from the observational analyses do not depend on the time since the air parcel exited
684 the storm core and was sampled by the DC-8 aircraft (Figure 7c), which was determined from
685 the distance the aircraft was from the storm core using Figure 2 and dividing by the horizontal
686 wind speed from the aircraft measurements. Indeed, the storms with the highest CH₃OOH
687 scavenging efficiencies, June 6 and May 29, have very different estimated times since the air
688 parcel exited the storm core of ~60 minutes and ~18 minutes, respectively.

689
690 Aqueous-phase chemistry can also affect CH₃OOH mixing ratios in a storm via in-cloud reaction
691 between CH₃OOH and HSO₃⁻ [Seinfeld and Pandis, 1998],



693 The hydroxyl radical OH can also oxidize CH₃OOH in the aqueous phase forming either CH₃OO
694 radicals or CH₂O.



697 Barth et al. [2007a] included reactions A2 and A3 in their cloud chemistry modeling of
698 thunderstorm chemistry and found essentially the same scavenging efficiency when aqueous
699 chemistry was included in the simulation as when aqueous chemistry was excluded. However,
700 Barth et al. [2007a] did not include reaction A1. To learn whether reaction A1 may be important,
701 the CH₃OOH scavenging efficiency is compared to the SO₂ inflow mixing ratios for each storm
702 case. Unfortunately SO₂ mixing ratios from the DC-8 are not available for the May 29 Oklahoma
703 storm because of instrument problems that day. The GV SO₂ measurements at low levels (2-3.5
704 km altitude) were obtained just before storm initiation but were primarily in western Oklahoma,
705 to the west of where the DC-8 inflow legs were. Thus, the low-level GV measurements were not

706 necessarily representative of the inflow conditions and are not used here. A comparison of the
707 CH₃OOH scavenging efficiencies with inflow SO₂ for the other five storm cases shows a strong
708 anti-correlation, with more scavenging at low SO₂ conditions (Figure 7d). Intuitively, this anti-
709 correlation seems to be the opposite of what is expected if aqueous-phase chemistry is reducing
710 CH₃OOH. While there is a strong anti-correlation between CH₃OOH scavenging efficiencies and
711 inflow SO₂, it is not obvious if SO₂ is affecting CH₃OOH mixing ratios in the storm outflow
712 region.

713

714 **5. Conclusion**

715 We have analyzed DC3 observations of hydrogen peroxide and methyl hydrogen peroxide to
716 determine their scavenging efficiencies in thunderstorms observed in the High Plains of northeast
717 Colorado and Southern Great Plains of Oklahoma. The analysis method, which is similar to that
718 described by Fried et al. [2015], first finds an entrainment rate for each storm by using mixing
719 ratios of n-butane, i-butane, n-pentane, and i-pentane, which are all sufficiently long-lived
720 chemically and insoluble to be good tracers of transport, in the inflow and outflow regions, and
721 clear-air vertical profiles. Once the entrainment rate is known, the peroxide scavenging
722 efficiencies are found from the measurements from the same inflow, outflow, and clear-sky
723 regions. The calculated H₂O₂ and CH₃OOH scavenging efficiencies are 79-97% and 12-84%,
724 respectively, for six DC3 storms analyzed. The scavenging efficiency uncertainties are 5-23%
725 and 15-67% for H₂O₂ and CH₃OOH, respectively, and are mostly from the uncertainties of the
726 peroxide measurements. The cloud resolving modeling by Bela et al. [2015] predicts scavenging
727 efficiencies similar to those observed for the 29 May 2012 DC3 storm when the retention
728 efficiency of H₂O₂ and CH₃OOH dissolved in freezing drops was 25% or greater for H₂O₂ and

729 100% for CH₃OOH. These modeling results suggest that the degree of riming of cloud drops by
730 snow and graupel could affect the amount of CH₃OOH scavenged by the storms.

731

732 We investigated several environmental, storm morphology, and chemical parameters that may
733 contribute to the wide range of calculated CH₃OOH scavenging efficiencies. While the
734 thermodynamic environment (e.g. CAPE and 0-6 km vertical wind shear) and physical processes
735 (e.g. ice water content) play a role in the degree of scavenging, they do not explain why
736 CH₃OOH scavenging has such a large range for the six storms examined. We found that more
737 CH₃OOH was scavenged at low entrainment rates and less CH₃OOH was scavenged at high
738 entrainment rates in storms. This correlation may be connected with the shape of the CH₃OOH
739 vertical profile in clear sky since the peroxide profiles usually did not decrease sharply with
740 altitude like the butane and pentane vertical profiles, from which the entrainment rate was
741 derived. Further, the variability of entrainment rate with height (as prescribed by the cloud
742 resolving model simulation) does not significantly change the calculated scavenging efficiencies.

743

744 The production of NO from lightning may influence CH₃OOH mixing ratios in the convective
745 outflow by increasing the CH₃OO + NO and the CH₃OO + NO₂ reaction rates, which reduces the
746 production of CH₃OOH via CH₃OO + HO₂. Correlations between the CH₃OOH scavenging
747 efficiency and the fraction of CH₃OO producing CH₃OOH and between the scavenging
748 efficiency and methyl peroxy nitrate suggest such a connection. However, our gas-aqueous
749 photochemical box model shows that gas-phase CH₃OOH mixing ratios are unchanged when a
750 NO source is included in the simulation. CH₃OOH can also be destroyed in the aqueous phase
751 via reaction with bisulfite ion (the dominant form of SO₂ in cloud droplets), suggesting a positive

752 correlation between CH_3OOH scavenging efficiencies and the inflow SO_2 mixing ratios.
753 However, we found a strong anti-correlation between these two quantities indicating that the
754 aqueous-phase chemistry may not contribute to the wide range of scavenging efficiencies found.

755

756 The analysis done here, via correlations between measured variables and calculated scavenging
757 efficiency and process-scale modeling, suggests that dynamical, physical, and chemical
758 processes affect CH_3OOH in the outflow of thunderstorms. The amount of hail in the storm plays
759 an important role in two ways. First, the production of hail involves substantial riming of cloud
760 droplets by falling snow and graupel. A portion of a trace gas dissolved in the cloud droplets
761 would be retained in the precipitating hail and subsequently removed from the atmosphere. Hail
762 also plays a key role in triggering lightning. The NO produced from lightning reduces the
763 production of gas-phase CH_3OOH because of NO and NO_2 reactions with CH_3OO (a key
764 precursor of CH_3OOH) forming formaldehyde, NO_2 , and methyl peroxy nitrate, as shown in
765 scatter plots between CH_3OOH scavenging efficiencies and two of these parameters. However,
766 photochemical box model simulations do not confirm that increased NO causes decreased
767 CH_3OOH mixing ratios at the top of the storm core. This investigation provides guidance for
768 future studies on understanding the complex interactions between storms and chemistry for
769 peroxides. To more thoroughly understand these interactions, cloud chemistry modeling that
770 explores the various effects of entrainment, hail (especially its role in scavenging soluble trace
771 gases via the riming of cloud droplets), lightning- NO_x , and other chemistry precursors should be
772 pursued.

773

774 Previous studies estimated CH₃OOH scavenging efficiencies to be <10%, thus the high values
775 found in this study are surprising and could have implications on the chemistry downwind of
776 convection in the upper troposphere. The low CH₃OOH mixing ratios (100-350 pptv) in the
777 convective outflow observed here would produce via CH₃OOH photolysis and OH oxidation less
778 CH₂O and HO_x radicals than if less CH₃OOH were scavenged. Thus, the high scavenging
779 efficiencies of CH₃OOH may explain discrepancies between photochemical box model
780 calculations and measurements of CH₂O in convective outflow plumes, similar to those
781 described by Fried et al. [2003]. It is expected that the low H₂O₂ and CH₃OOH mixing ratios in
782 the convective outflow would have a smaller contribution to downwind O₃ production compared
783 to CH₂O, whose mixing ratios in the convective outflow ranged from 600 to 1500 pptv [Fried et
784 al., 2015]. The contribution of CH₂O and the peroxides to UT O₃ formation can be pursued
785 further via model calculations.

786

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1113 **Tables**

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1116 **Table 1.** List of data and instruments used in the analysis.

Species/Parameter	Instrument ^a	Uncertainty
H ₂ O ₂ , CH ₃ OOH	CIT-CIMS	H ₂ O ₂ (pptv): 75 + 0.5 [H ₂ O ₂] CH ₃ OOH (pptv): 30 + 0.4[CH ₃ OOH] at H ₂ O vapor < 230 ppmv 30 + (-9.1+log ₁₀ [H ₂ O]) [CH ₃ OOH] at H ₂ O vapor > 230 ppmv
n-butane, i-butane, n-pentane, i-pentane	WAS	5% or 3 pptv
NO, NO ₂ ^b	CSD CL	NO (pptv): 10 + 0.04 [NO] NO ₂ (pptv): 20 + 0.06 [NO ₂]
NO ₂ , MPN ^c	TD-LIF	NO ₂ : 5% MPN: 40%
OH, HO ₂	ATHOS	32%
SO ₂	GT-CIMS	15%
H ₂ O vapor	DLH	5% or 1 ppmv
Pressure, Temperature, 3D Winds	MMS	Pressure: 0.5% Temperature: 0.2% Winds: 3%
Ice water content	2DS	Not available

1117 ^aCIT-CIMS is California Institute of Technology chemical ionization mass spectrometry; WAS is the
 1118 Whole Air Sampler that uses gas chromatography; CSD CL is NOAA Chemical Science Division
 1119 chemiluminescence; TD-LIF is thermal dissociation – laser induced fluorescence; ATHOS is Airborne
 1120 Tropospheric Hydrogen Oxides Sensor that uses laser induced fluorescence; GT-CIMS is Georgia
 1121 Institute of Technology chemical ionization mass spectrometry; DLH is diode laser hygrometer that uses
 1122 differential absorption spectroscopy; MMS is Meteorological Measurement System; 2DS is two-
 1123 dimensional stereo probe.

1124 ^bThe NO₂ measurement should be interpreted as the sum of NO₂ and MPN based on the findings of
 1125 Browne et al. [2011].

1126 ^cMPN is methyl peroxy nitrate.

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Table 2. DC3 cases investigated.

Date	Location	CAPE (J kg⁻¹)	0-6 km Vertical Wind Shear (m s⁻¹)	Cloud base to Freezing Level Depth (m)	Freezing Level to -40°C Depth (m)
18 May 2012	Southwest Nebraska	1144	12.1	121	4910
29 May 2012	Northern Oklahoma	3113	19.0	2505	5780
02 June 2012	Northeast Colorado	918	13.2	640	5172
06 June 2012	Northeast Colorado	2981	17.5	1157	5145
16 June 2012	Central Oklahoma	3049	15.9	2762	5803
22 June 2012	Southwest Nebraska	2563	24.2	1750	5229

Table 3. Inflow and outflow times (UTC) and altitude (km, MSL) of measurements from the DC-8 aircraft used for analysis.

Date	Inflow Time (UTC)	Inflow Altitude (km)	Outflow Time (UTC)	Outflow Altitude (km)
18 May 2012	22:48:29-22:51:10	1.7	23:17:50-23:22:00	11.3
29 May 2012	23:10:21-23:15:53	1.3	23:49:18-23:58:13	11.0
02 June 2012	21:16:18-21:27:38	1.9	22:40:46-22:46:10	11.1
06 June 2012	22:13:40-22:25:12	1.7	23:57:22-24:01:59	12.4
16 June 2012	24:15:00-24:20:00	0.95	25:50:00-25:55:00	11.9
22 June 2012	22:31:27-22:45:54	2.0	25:16:51-25:19:24	11.2

Table 4. Configuration of the WRF simulation.

Process	Parameterization	Reference
Meteorology Initialization	North American Mesoscale Analysis with pre-storm lightning data assimilation	Fierro et al. [2012]
Cloud microphysics	Morrison 2-moment	Morrison et al. [2009]
Deep/shallow convection	none	
Planetary boundary layer	YSU ^a	Hong et al. [2006]
Land surface	Noah	
Short/longwave radiation	RRTMG ^b	Iacono et al. [2008]
Chemistry Initialization	Combination of aircraft measurements and MOZART global chemistry transport model	Bela et al. [2015] Emmons et al. [2010]
Anthropogenic Emissions	EPA NEI 2011	
Biogenic Emissions	MEGAN ^c v2.04	Guenther et al. [2006]
Biomass Burning Emissions	FINN ^d	Wiedinmyer et al. [2011]
Gas-phase Chemistry Mechanism	MOZART ^e	Emmons et al. [2010]
Aerosol Physics and Chemistry	GOCART ^f	Chin et al. [2002]
Dry Deposition	Resistance method	Wesely [1989]
Wet Deposition	Henry's Law equilibrium with net production of precipitation	Neu and Prather [2012]

^aYSU = Yonsei University scheme; ^bRRTMG = Rapid Radiative Transfer Model for GCMs; ^cMEGAN = Model of Emissions of Gases and Aerosols from Nature; ^dFINN = Fire Inventory from NCAR; ^eMOZART = Model for Ozone and Related Chemical Tracers; ^fGOCART = Goddard Chemistry Aerosol Radiation and Transport model.

Table 5. Percent contributions of each 1-km altitude layer to the storm core top as determined from the WRF-Chem simulation.

Layer Bottom Altitude (km)	Layer Top Altitude (km)	Percent Contribution (%)
0	1	6.4 ± 4.8
1	2	12. ± 7.8
2	3	9.4 ± 5.5
3	4	5.0 ± 3.1
4	5	5.8 ± 3.6
5	6	8.5 ± 5.7
6	7	9.4 ± 6.7
7	8	8.4 ± 5.9
8	9	8.3 ± 7.9
9	10	5.7 ± 12.
10	11	0.26 ± 0.86
11	12	0.01 ± 0.02
Average for 1-11 km altitudes		7.3 ± 3.3

Table 6. Mixing ratios of H₂O₂ (pptv) and CH₃OOH (pptv) averaged for the inflow and outflow times. The uncertainties of the average values are included.

Date	Inflow Time		Outflow Time	
	H ₂ O ₂	CH ₃ OOH	H ₂ O ₂	CH ₃ OOH
18 May 2012	665±407	571±453	87±119	102±71
29 May 2012	2462±1306	1522±1276	169±160	175±104
02 June 2012	2108±1129	580±459	60±105	199±109
06 June 2012	4135±2142	1148±911	94±122	126±81
16 June 2012	1777±964	1655±1381	90±120	336±164
22 June 2012	1544±847	647±499	255±203	276±145

Table 7. Mixing ratios of n-butane, i-butane, n-pentane, i-pentane (pptv) and the i-butane/n-butane and i-pentane/n-pentane ratios averaged for the inflow and outflow regions. The standard deviations of the averages are included.

Date	Inflow Region		Outflow Region		Inflow	Outflow
	n-butane	i-butane	n-butane	i-butane	i-butane/n-butane	
18 May 2012	1511±45	537±16	431±65	164±23	0.36	0.38
29 May 2012	1548±31	513±10	763±61	280±25	0.33	0.37
02 June 2012	262±68	112±25	108±3	51±3	0.43	0.48
06 June 2012	312±28	132±10	224±2 ^a	95±4 ^a	0.42	0.39
16 June 2012	1746±514	678±165	406±39	169±19	0.40	0.42
22 June 2012	194±25	70±11	150±3	52±3	0.36	0.35
	n-pentane	i-pentane	n-pentane	i-pentane	i-pentane/n-pentane	
18 May 2012	365±11	377±11	107±17	110±18	1.03	1.03
29 May 2012	457±9	397±8	202±17	210±26	0.87	1.04
02 June 2012	68±19	72±25	31±3	32±3	1.05	1.02
06 June 2012	80±8	84±13	56±1 ^a	54±1 ^a	1.05	0.96
16 June 2012	596±202	550±145	105±21	109±18	0.92	1.04
22 June 2012	44±4	49±5	42±3	34±3	1.11	0.81

^aValues from Fried et al. [2015] using the outflow measurements from both the DC-8 and GV. These values are extrapolated to the top of the storm core as described by Fried et al. [2015].

Table 8. Entrainment rate and scavenging efficiencies for each storm analyzed.

Date	Entrainment Rate (% km⁻¹)	Scavenging Efficiencies (%)	
		H₂O₂	CH₃OOH
18 May 2012	14.1 ± 0.3	84 ± 23	58 ± 35
29 May 2012	7.6 ± 1.6	88 ± 11	77 ± 20
02 June 2012	16.5 ± 4.6	94 ± 13	12 ± 67
06 June 2012	4.1* ± 0.7	97 ± 05	84 ± 15
16 June 2012	17.2 ± 1.7	89 ± 15	30 ± 50
22 June 2012	4.8 ± 0.9	79 ± 19	44 ± 47

*Entrainment rate is from Fried et al. [2015].

Figures

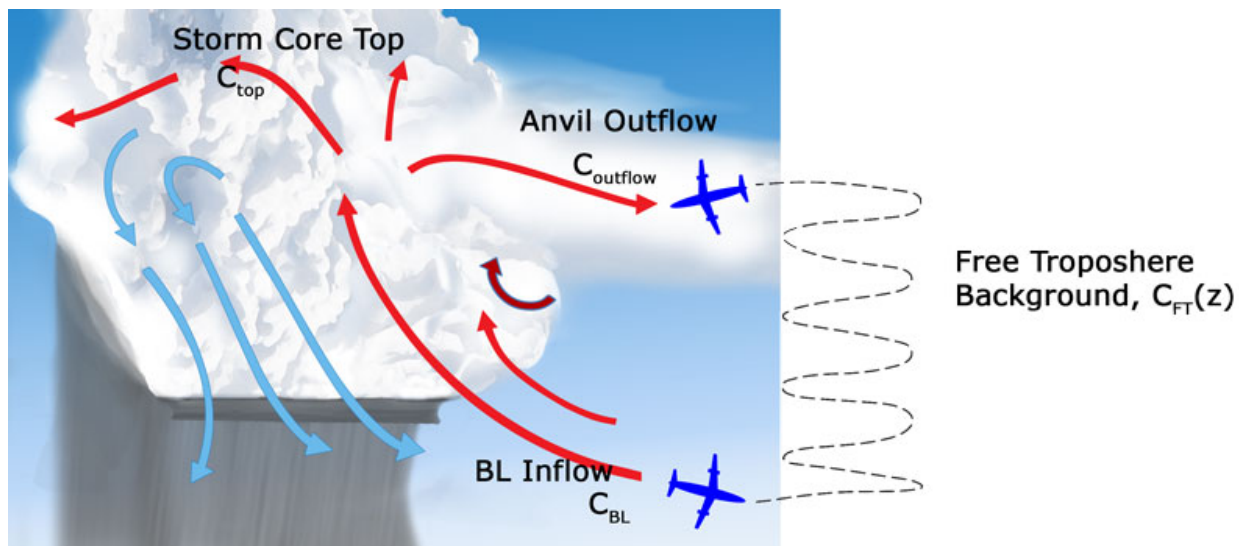


Figure 1. Air motions associated with deep convection in an environment with high vertical wind shear. The schematic is annotated with locations of the measured trace gas mixing ratios in the boundary layer inflow, free troposphere background, anvil outflow, and storm core top. Also shown is a schematic of the DC-8 flight pattern for sampling clear air profiles near the thunderstorm.

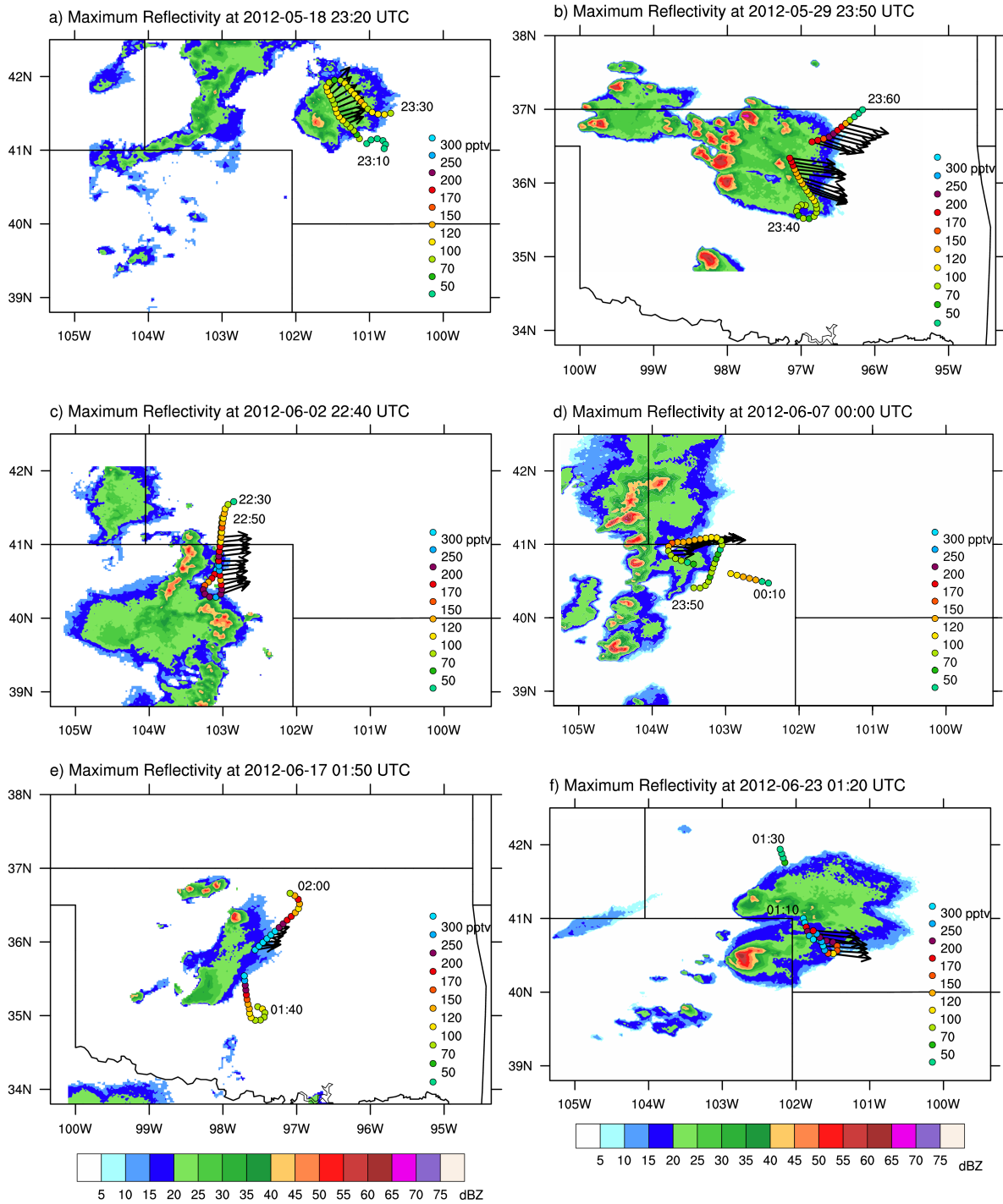


Figure 2. Maximum column reflectivity from the NWS NEXRAD radars for a) 18 May southwest Nebraska, b) 29 May Oklahoma, c) 2 June Colorado, d) 6 June Colorado, e) 16 June Oklahoma, and f) 22 June Colorado DC3 cases. Overlaid is the NASA DC-8 aircraft flight track with the start and end times of the outflow flight leg and colored by the mixing ratio of CH_3OOH (pptv) for the 20 minutes surrounding the time of the radar reflectivity image. Vectors indicate the aircraft winds for times when outflow data were used for the scavenging efficiency calculation.

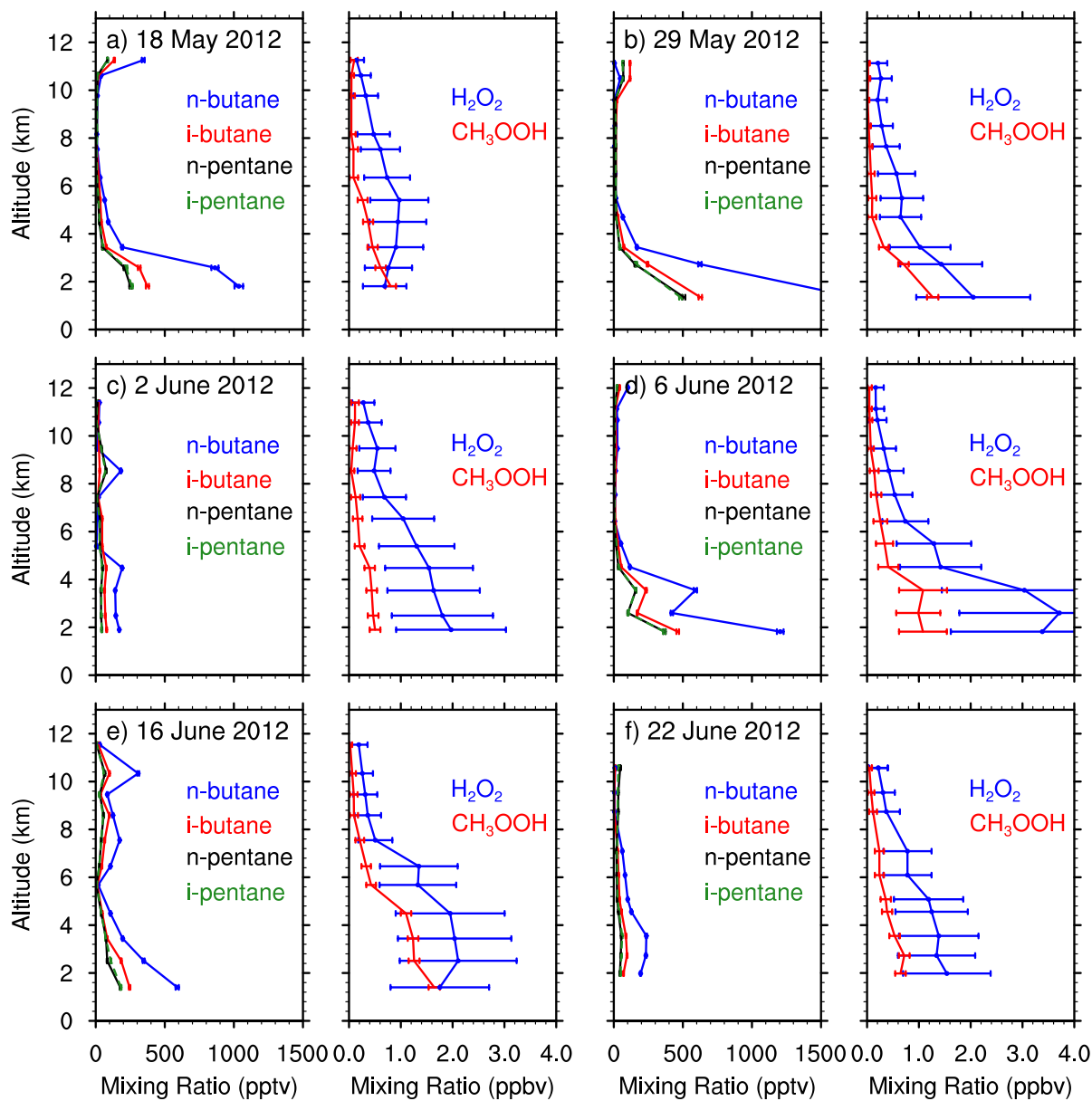


Figure 3. Cloud-free vertical profiles of n-butane (blue), i-butane (red), n-pentane (black), i-pentane (green), and H_2O_2 (blue) and CH_3OOH (red) for the a) 18 May, b) 29 May, c) 2 June, d) 6 June, e) 16 June, and 22 June 2012 DC3 cases.

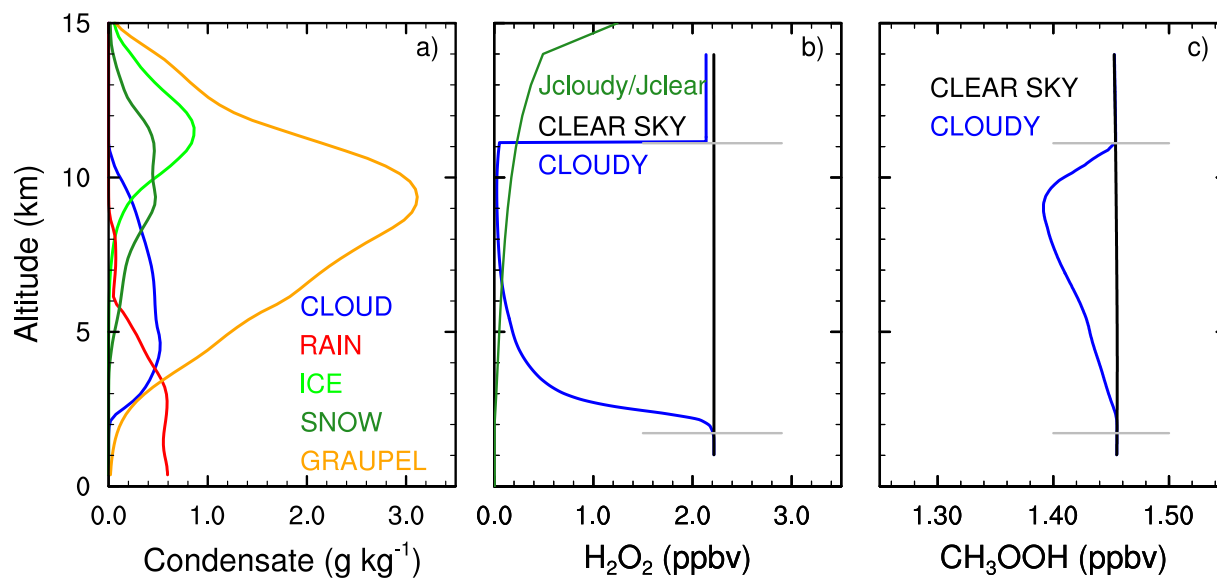


Figure 4. Vertical profiles of a) storm hydrometeor mixing ratios obtained from the WRF-Chem simulation, and gas-phase b) H_2O_2 and c) CH_3OOH mixing ratios calculated by the gas-aqueous photochemical box model. In panel a), cloud water is the blue line, rain the red line, ice the green line, snow the dark green line, and graupel/hail the orange line. In panels b) and c), the gas chemistry only simulation is the black line, and the gas-aqueous chemistry is the blue line and used the cloud water mixing ratios shown in a). The cloud water base and top are marked by the horizontal gray lines. In b) the ratio of the cloudy to clear sky H_2O_2 photolysis rate at 00 UTC is shown in dark green.

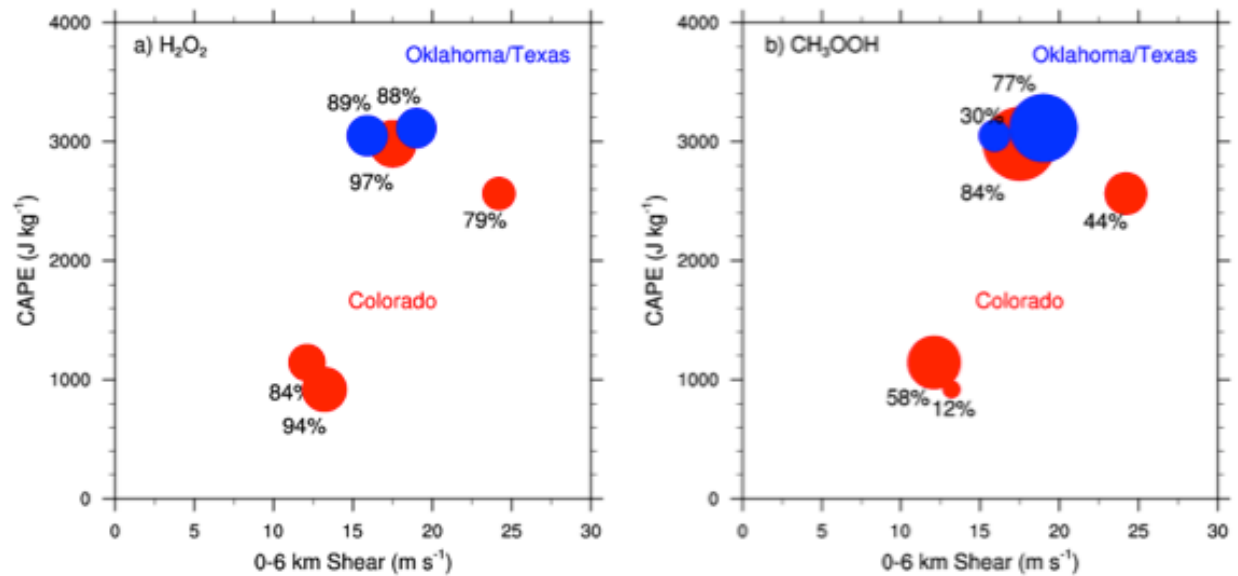


Figure 5. Scavenging efficiencies of H₂O₂ (a) and CH₃OOH (b) placed in the CAPE – low-level vertical wind shear parameter space. The size of the circles is scaled to the scavenging efficiency values. Blue circles denote Oklahoma storms and red circles are Colorado storms.

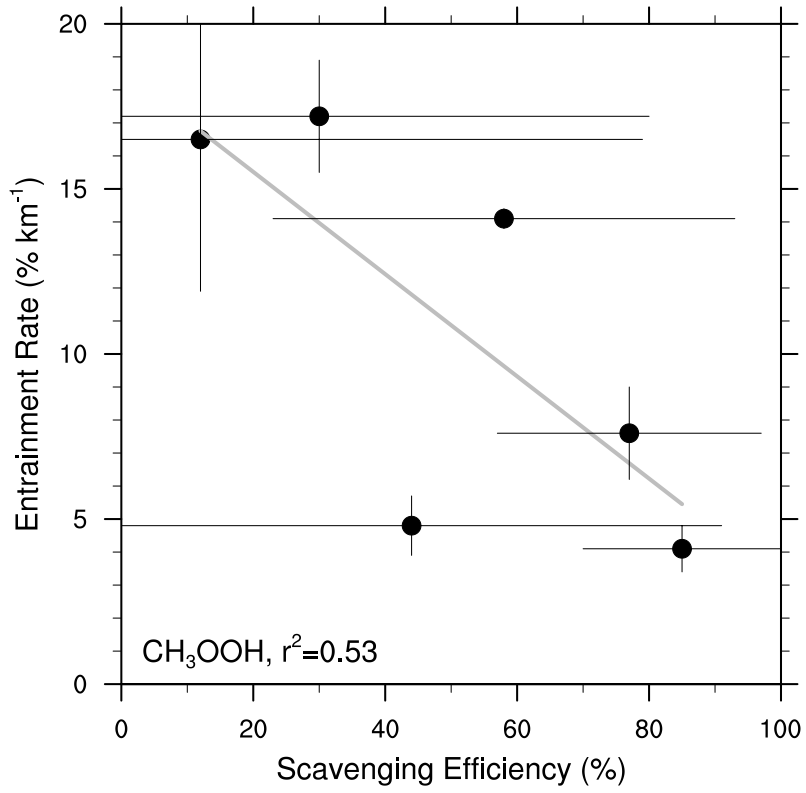


Figure 6. Correspondence of estimated CH₃OOH scavenging efficiencies and storm entrainment rates. The gray line in each plot represents the regression line for the data shown.

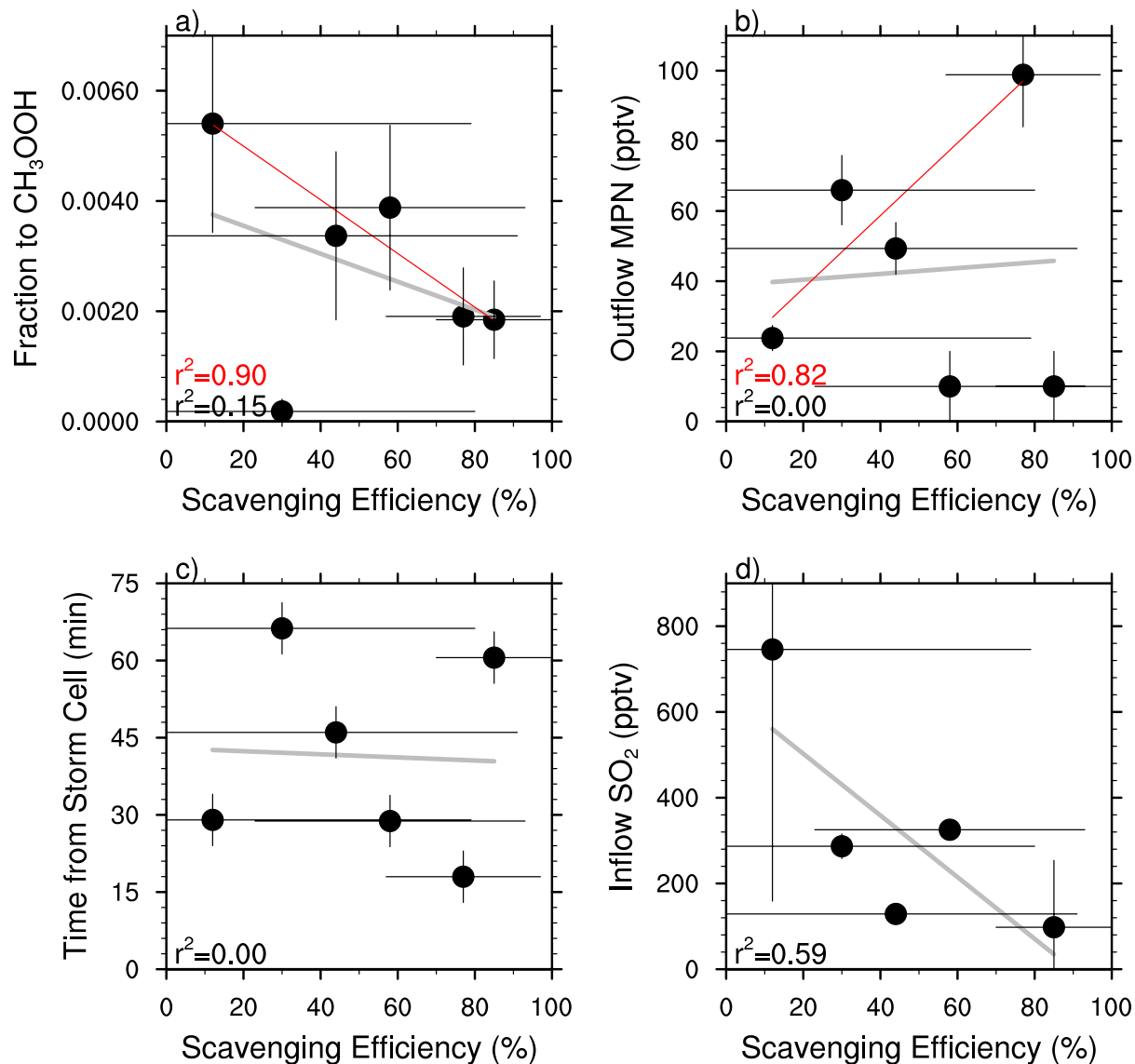


Figure 7. Correspondence of CH_3OOH scavenging efficiency with estimated a) fraction of CH_3OO producing CH_3OOH , b) 60-s averaged methyl peroxy nitrate data in the outflow flight leg, c) time traveled by sampled air from storm cell to the aircraft in the outflow region, and d) average SO_2 mixing ratio in the inflow region of the storm. See text for details on how each parameter was estimated. The gray line in each plot represents the regression line for the data shown. The red line in panels a) and b) represents the regression line for the data without the 16 June data point and without the 18 May and 6 June data points, respectively.

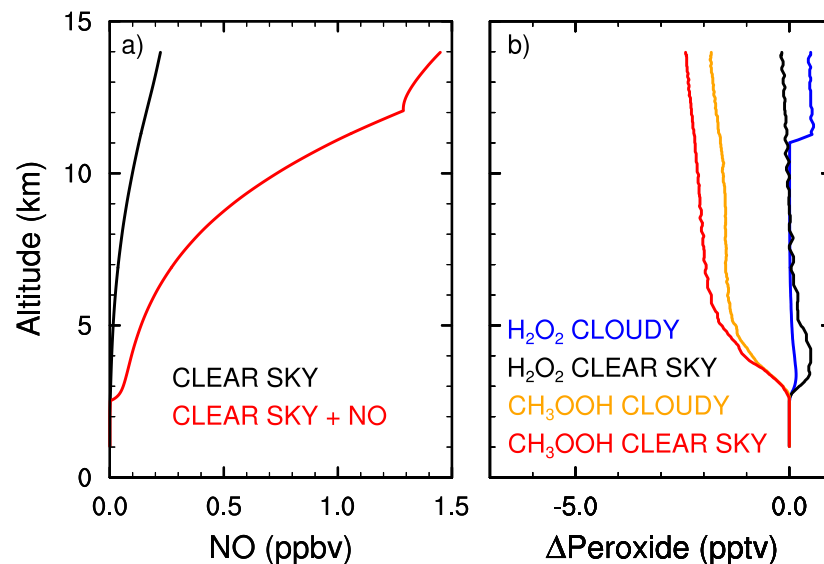


Figure 8. Vertical profiles of gas-phase a) NO calculated by the photochemical gas-aqueous chemistry box model, and b) the difference between gas-phase H_2O_2 and CH_3OOH mixing ratios between the simulations with and without the NO source. The black and blue lines are H_2O_2 differences from the gas-only chemistry and gas-aqueous chemistry simulations, respectively. The red and orange lines are CH_3OOH differences from the gas-only and gas-aqueous chemistry simulations, respectively.